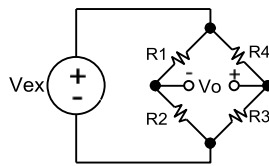


The Wheatstone Bridge

$\Delta R = R * GF * \epsilon$ implies that at $3000\mu\epsilon$, $\Delta R/R \sim 2.00 * 3000 * 10^{-6} = 0.006$ or 0.6%

We stated that because strain measurement requires the detection of very small resistance changes resulting from very small mechanical deformations, we wire strain gauges as elements of a Wheatstone bridge which converts the signal to a bipolar output voltage that can be conveniently measured in proportion to the applied stress and its direction. Note that the magnitude of most strain measurement in stress applications is commonly between $2000\mu\epsilon$ and $10000\mu\epsilon$, and rarely larger than about $3000\mu\epsilon$ or $\sim 0.6\%$. The Wheatstone Bridge offers an accurate method for measuring these very small changes in resistance and even provides an ability to compensate for the inherent sensitivity of the strain gauge relative to temperature.

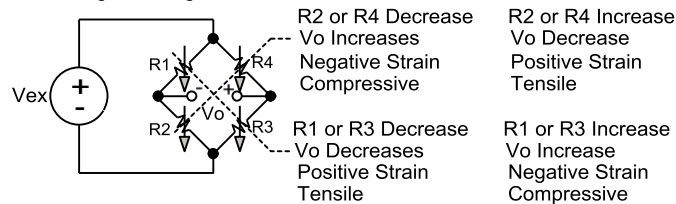
Figure 1: Wheatstone Bridge



The Wheatstone Bridge is comprised of four resistive arms or bridge elements arranged in the configuration of a diamond as shown at left. An excitation voltage V_{ex} is applied vertically across the diamond or bridge input and an output voltage V_o can be measured horizontally across the diamond as shown in Figure 1.

From Kirchoff's Voltage Law & Ohm's Law, the bridge output voltage V_o is the difference between two divided voltages with $V_o = [R3/(R3+R4) - R2/(R2+R1)] * V_{ex}$. If the adjacent resistors of each divider match their ratios such that $R1/R2 = R4/R3$, then $V_o=0$ and the bridge is *balanced*. Note it is not required that $R1=R4$ and $R2=R3$ to achieve balance, just that the ratios of adjacent resistors $R1:R2$ and $R4:R3$ be equal (this also allows you to use half bridge completion resistors of a different value than the nominal gauge resistance). But for simplicity, if all four of the resistances in each leg of the bridge are equal, the two divider pairs will have equal ratios and the bridge will be balanced with a bridge output voltage $V_o=0$. Any change in resistance in any leg of the bridge will unbalance the bridge and produce $V_o \neq 0$. Remember that the same V_o can be obtained from adjacent pairs of different resistor values, if the ratios of the adjacent pairs are kept equal ($R1/R2 = R4/R3$).

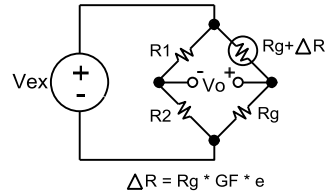
Figure 2: Sign Convention



As stated, if $R1/R2 = R4/R3$, then $V_o=0$ and the bridge is balanced. Examine the two V_{ex} voltage dividers $V_{o-} = R2/(R1+R2) * V_{ex}$ and $V_{o+} = R3/(R4+R3) * V_{ex}$. Note a decrease in $R4$ or $R2$ increases V_o by increasing the +node voltage and decreasing the -node voltage. Likewise, a decrease in $R1$ or $R3$ will decrease V_o by increasing the -node voltage and reducing the +node voltage. The strain due to a decrease in resistance $R4$ or $R2$ will be negative and increase V_o (convention is that negative strain is compressive and positive strain is tensile). Thus, bridge V_o will grow positive for a compressive stress on $R4$ driving negative strain and decreasing its resistance. This is the convention used throughout this manual.

Wheatstone Bridge...

Figure 3: Strain Bridge w/ Gauge Factor



If you replace R_4 in the bridge with an active strain gauge (R_g), then any change in the strain gauge resistance (ΔR) will unbalance the bridge and produce an offset in V_o proportional to the change in resistance ΔR . Using Gauge Factor, the change in resistance due to the applied strain is $\Delta R = R_g * GF * \epsilon$.

From our divider equation $V_o = V_{ex} * [R_3 / (R_4 + R_3) - R_2 / (R_1 + R_2)]$, substituting $R_1 = R_2$, $R_3 = R_g$, and $R_4 = R_g + \Delta R$ yields: $V_o / V_{ex} = -GF * \epsilon / 4 * [1 / (1 + GF * \epsilon / 2)]$. This is the strain computation term $V_r = V_o / V_{ex}$ in mV/V and represents the *sensitivity* of the bridge network in mV/V (not to be confused with strain gauge sensitivity or Gauge Factor). The presence of the extra term $1 / (1 + GF * \epsilon / 2)$ is representative of a small non-linearity in the output of the quarter bridge network with respect to strain. But for quarter-bridge strain levels below ~5000 micro-strain, the effect of this non-linearity is small and can be ignored in most applications.

Strain sensors formed from a bridge network may employ multiple strain gauges in their construction with 1, 2, or 4 active gauges in a bridge possible. Note that one active strain gauge (R_g) may occupy one leg of a four element Wheatstone Bridge (Quarter-Bridge), two legs of a bridge (Half-Bridge), or four legs of a bridge (Full-Bridge). Any remaining legs of a quarter or half bridge network are occupied by fixed resistors or "dummy" gauges, but it is the number of active gauges in the bridge that determines whether the bridge is a quarter (1), half (2), or full bridge (4) type.

Refer back to Figure 2 and note that tensile (positive) strain drives negative V_o for elements 1 and 3, and elements 4 and 2. Compressive (negative) strain drives V_o positive for 1 and 3, and elements 2 and 4. A change of resistance in the same direction for adjacent bridge resistors is subtractive and tends to cancel each other out, but a change of resistances in opposite directions for adjacent cells is additive and reinforces their effect on the output V_o . Similarly, resistance changes between diagonally opposite resistors are additive in same direction and reinforce their effect on output V_o , but subtractive in opposite directions and tend to cancel each other out.

Because strain gauges are inherently sensitive to temperature, we can additionally arrange them in a bridge to compensate its V_o for temperature by making sure the adjacent element pair ratios $R_1 : R_2$ and $R_3 : R_4$ remain equal over temperature. Because opposite changes in resistance of adjacent bridge resistors R_1 & R_2 and R_3 & R_4 are numerically additive and reinforce each other, but numerically subtractive if in the same direction, then placing similar gauges and lead-wires in adjacent arms and exposing them to the same temperature will allow them to act together to null the net thermal effect on the bridge output V_o and effectively cancel temperature induced strain error.

That is, for an active strain gauge in one arm, use an identical strain gauge in the adjacent arm, subject to the same temperature but not the stress force. Then its temperature resistance change will track that of the primary gauge, and the ratio between them will stay the same, having no unbalancing effect on the bridge output V_o signal.

Application

Strain gauge elements are arranged in bridge networks to measure strain or load on a material relative to bending, axial, shear, and torsion. A material under load that extends in the direction of applied stress normally exhibits longitudinal tensile strain and coincident strain in the transverse or lateral direction that is contractive for most materials (Poisson's strain).

Bending stress results when a beam with a straight horizontal (longitudinal) axis is loaded by a lateral/transverse force such that its longitudinal axis bends into a curve. This strain is used to determine vertical loads.

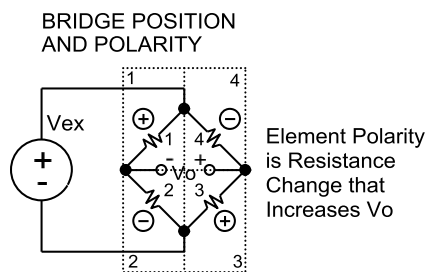
Axial stress/strain results when a body becomes shorter (compressive) or longer (tension) along the direction of an applied force. This strain is used to determine axial loads via material elongation.

Shear strain is the ratio of change in deformation to original dimensions along the length or axis perpendicular to the cross-section of the body (it's the stress parallel to the cross section of the body). Shear stress drives deformation of a material by causing slippage along a cross-sectional plane parallel to the applied stress. For example, when a shear is used to cut a piece of material, the upper and lower parts of the shear exert lateral loads on the material that drives shear stress in it, causing it to separate into cross-sectional planes. Shear strain is defined as the tangent of the angle and is equal to the length of deformation at its maximum (45°) divided by the perpendicular length in the plane the force is applied. Torsional strain is a form of shear stress that results from an object twisted about an axis such that both tensile and compressive stresses are simultaneously imposed that can cause shear.

A detailed discussion of stress applications is beyond the scope of this document, except to say that specific bridge types are used for specific stress applications with bending and axial stress measurement the most common.

Most strain instruments will support all Wheatstone Bridge based sensor types incorporating separate strain gauges wired in a bridge for strain measurement, or simple load cells that utilize a Wheatstone Bridge internally and are used for measuring force (pressure transducers, torque converters, accelerometers, and vibration sensors). In general, the input to the strain instrument requires the input to be wired as a complete bridge circuit (4 wire nodes) plus remote sense lines to the bridge excitation nodes (6 wires total). But regardless of the sensor type, the strain module needs two measurements to resolve the corresponding strain or load: sensor output V_o and sensor excitation V_{ex} .

Load cell sensors may operate under compression and/or tension and will yield bipolar or unipolar millivolt output voltage V_o directly proportional to the applied force. Its output reading is often expressed in percent of span/full-load, and this can be easily scaled to other units using software gain. Load cells may already be internally compensated for temperature changes and their use does not require you to know additional details of its internal bridge, sensor Gauge Factor, or material Poisson's ratio. Only the rated output and nominal excitation are considered for load cells.



- + Strain is Tensile (Elongation)
- Strain is Compressive (Contraction)
- Same Diagonal Polarity Adds to V_o
- Opposite Adjacent Polarity Adds to V_o

For a strain bridge, its formulation is more complex and requires knowledge of other parameters and the application. For any bridge, you must know the number of active load cells to determine whether it is a quarter (1), half (2), or full (4) bridge. Additionally, you must discern its specific type number by considering the way additional gauges are mounted in the bridge (their purpose), whether a “dummy” gauge is present, and whether half-bridge completion resistors are included or built into the sensor.

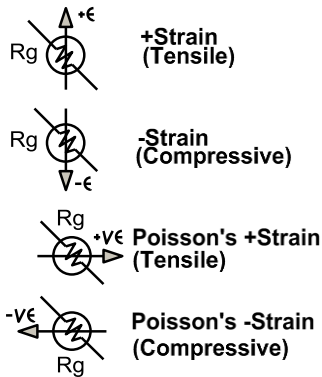
Generally, for connecting to a strain gauge bridge, the instrument is considered an *indicator* for measured strain and internally may refer to two values of strain—the ideal or simulated strain of which its computation uses the actual sensor Gauge Factor and a Software Gain of 1, and a calculated or indicated strain which substitutes your Instrument Gauge Factor and/or optional Software Gain that you control to rescale its indication for your

application. In most applications, simulated strain and indicated strain are driven to converge using calibration tools built into the instrument that adjust Instrument Gauge factor and/or gain to alter the indicated value.

Strain Bridge Equations

The strain bridge formulas that follow are used to compute both *ideal or simulated strain* and *indicated strain*. For Indicated Strain, your Instrument Gauge Factor will be substituted for Gauge Factor (initial IGF ~ 2) and/or your result may be subject to software gain that you specify to rescale Indicated Strain or Load during shunt or load calibration, typically to resolve application inefficiencies between the ideal and indicated strain or load.

Bridge Figure Key:



An active strain gauge measures axial strain when mounted in the same direction as the applied force and bending strain when mounted in a lateral direction to the applied force.

Table 1 reviews the terms and nomenclature used in the subsequent strain and load cell formulas for various strain gauge bridge configurations and for load cells.

Table 1: Strain and Load Parameters

Parameter	Definition
Vo <i>Bridge Output</i>	<u>ADC Measurement 1</u> – Sensor Bridge Output Voltage V_o . To account for the non-balance $V_o \neq 0$ offset condition of an unstrained bridge, a distinction is made for V_o via $V_{o_strained}$ for the bridge output under load, and $V_{o_unstrained}$ for the bridge output unloaded (initial bridge offset). Likewise, for any non-zero tare, $V_o = V_{o_loaded} - V_{o_unloaded} - V_{o_tare}$.
Vex <i>Bridge Excitation</i>	<u>ADC Measurement 2</u> - Bridge Excitation Voltage V_{ex} . This is normally derived from a related ADC measurement.
Vr <i>Bridge Sensitivity</i>	Key strain computation term that represents the sensitivity of the strain bridge and is derived from ADC measurements of V_o & V_{ex} with $V_r = (V_o \text{ strained} - V_o \text{ unstrained}) / V_{ex}$. It is equal to the bridge output signal per volt of excitation and expressed as mV/V.
GF (~2.00)	<i>Input Specification - Gauge Factor is the gauge specification for its sensitivity to strain (not the bridge sensitivity), ~2.00 for Metallic Gauges. $GF = (\Delta R / R) / (\Delta L / L) = (\Delta R / R) / \epsilon$, then $\Delta R = R * GF * \epsilon$</i>
RO (1-10mV/V)	<i>Input Specification - Rated Output (1-10mV/V) is the gauge specification for its output voltage range under full-load ($\pm 100\%$) per volt of applied excitation voltage.</i>
ϵ Strain +ϵ Tensile¹ -ϵ Compr¹	Strain ($\epsilon = \Delta L / L$, multiply by 10^6 for equivalent micro-strain). <i>tensile Strain ($\epsilon = +\Delta L / L$) and compressive strain ($\epsilon = -\Delta L / L$)</i>
γ	Poisson's Ratio, material constant w/ $-1 < \gamma < 0.5$ ($\gamma = -\epsilon_T / \epsilon$)
$\epsilon_T = -\gamma \epsilon$	Transverse (Poisson's) Strain
+$\gamma \epsilon$	A Tensile Poisson's strain $\gamma = -\epsilon_T / \epsilon$ & $\epsilon_T = -\gamma \epsilon$.
-$\gamma \epsilon$	A Compressive Poisson's strain $\gamma = -\epsilon_T / \epsilon$ & $\epsilon_T = -\gamma \epsilon$.
Rg	Nominal Strain Gauge Resistance (120 Ω , 350 Ω , 1000 Ω common).
RI	Lead-Wire Resistance
N	Common Factor used to Account for Multiple Gauges in a Bridge (see Table 2 for N value)

In the following examples, the polarities indicated assume a positive strain + ϵ is tensile and negative strain - ϵ is compressive, but you can reverse this convention by removing the negative sign from the strain formulas and flipping the polarity of the bridge output voltage V_o .

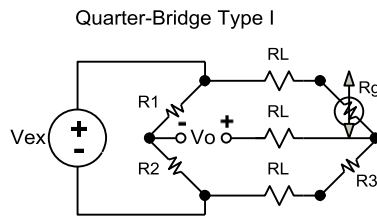
In the bridge, adjacent elements refer to the relationship between the two elements on the left, or the two elements on the right of a bridge. Diagonally opposite elements that measure strain in the same direction reinforce each other's effect on V_o , while adjacent strain gauges that measure in opposite directions reinforce each other's effect on V_o (they are additive to V_o). Adjacent gauges that are mounted transverse to primary $\pm \epsilon$ strain gauges normally measure the coincident Poisson's strain $\pm \nu \epsilon$.

Strain Bridge Equations...

Quarter Bridge Type I, N=1 (For Axial or Bending Strain)

One Active Gauge R_g with Dummy Resistor $R_3=R_g$ and Half-Bridge Completion Resistors $R_1=R_2$ and $R_1/R_2=R_g/R_3$.

Not Temperature Compensated



A quarter-bridge uses one active gauge R_g to make a uniaxial tensile or compressive strain measurement with the gauge mounted in the direction of an axial strain or transverse to a bending strain.

The Quarter Bridge is Type I is most common in experimental stress analysis, where

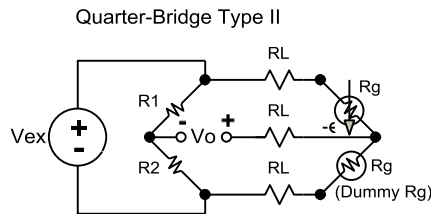
ambient temperature is relatively constant. It is not recommended for real world applications because it does not compensate for changes in temperature. In the Quarter bridge Type I configuration, the adjacent gauge resistor R_3 is only selected to have the same resistance as the strain gauge ($R_3=R_g$). The two resistors in the opposite half must equal each other ($R_1=R_2$), but do not have to equal to the gauge resistor R_g or R_3 , just their ratio ($R_1/R_2=R_g/R_3$).

Quarter-Bridge Type II, N=1 (For Axial or Bending Strain)

One Active Gauge R_g with Passive Gauge $R_3=R_g$ and Half-Bridge Completion Resistors $R_1=R_2$ and $R_1/R_2=R_g/R_3$.

Temperature Compensated

Good at lower levels of strain below $\sim 5000\mu\epsilon$ where Poisson's Strain is small.



A second Quarter Bridge is Type II and often used to measure compression, common to weigh-scale applications.

This quarter bridge uses one active gauge R_g , plus a transverse mounted passive "dummy" gauge to compensate for temperature. The dummy gauge is

not subject to strain and only provided for temperature compensation. Applied strain has little effect on a dummy gauge because it is mounted transverse/perpendicular to the applied force and normally unbonded to the application material, but close enough to the active R_g such that the ambient temperature affects both gauges equally maintaining their ratio but not affecting output V_o over temperature.

Note that the temperature compensated Quarter-Bridge (Type II) is sometimes incorrectly referred to as a half-bridge configuration due to the presence of the second gauge. But because the second gauge matches its TC to R_g but does not measure strain (it is not active), it is in fact a Quarter-Bridge Type II circuit and the quarter-bridge formulation applies (note the absence of Poisson's ratio). No quarter bridge formulation can be used in an application where the direction of the stress field is unknown or changes.

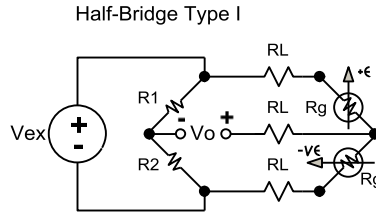
If any additional force is applied in the transverse direction of the dummy gauge, then the measurement of strain in the direction of the active gauge will be in error.

For Quarter-Bridge Type I or Type II, solving for the resultant strain will yield the following expression (note the absence of Poisson's Ratio because it is often ignored at lower levels of strain less than $\sim 5000\mu\epsilon$):

$$\epsilon = (1 + R_l/R_g) * -4V_r/[GF*(1+2V_r)]$$

Strain Bridge Equations...

Half-Bridge Type I, $N=1+\gamma$
(Single-Axis Strain Measurement at higher levels of stress)

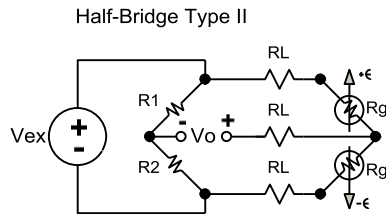


A Half-Bridge uses two active gauges in a single-axis (uniaxial) stress field to make strain measurements, one mounted in same direction as applied strain and the other mounted transverse to applied strain to capture the effect of Poisson's strain.

Solving for the strain of Half-Bridge Type I yields the following (note that Poisson's ratio is present because transverse strain is considered because of the generally higher stress levels): $\epsilon = -4Vr * (1 + Rl / Rg) / [GF*(1+\gamma) - 2Vr*(\gamma - 1)]$

The Half Bridge Type I resembles the Quarter-Bridge Type II, except that the transverse mounted gauge measures the transverse strain that results from its higher applicable stress levels where Poisson's strain is more significant. The secondary gauge still corrects for changing temperatures because of its matching temperature coefficient which keeps R3/R4 ratio constant over temperature.

Half-Bridge Type II, $N=2$
Bending Strain Only
(Bending Beam Applications at Lower Strain Levels)



The Half-Bridge Type II is typically used in bending beam applications. This bridge uses two active gauges with both subject to a bending stress, mounted to measure equal and opposite strain, one in compression (bottom of beam), one in tension (top of beam). Because the adjacent gauge pair

measures the same stress in opposite directions, their effect on Vo reinforces each other, doubling the output of the quarter bridge. The second gauge with a matching temperature coefficient also corrects for changes in temperature by keeping the gauge ratio R4/R3 constant. Solving for Half-Bridge Type II strain yields (note the absence of Poisson's Ratio suggests it is more applicable at lower levels of strain): $\epsilon = -2Vr *(1 + Rl / Rg) / GF$

Another permutation of this arrangement would have the two diagonally opposite active gauges subject to equal strain in the same direction (also reinforcing each other). For example, each gauge could be mounted on opposite sides of a column with a low thermal gradient between them (both subject to same temperature). Recall that diagonally opposite gauges reinforce each other for resistance changes in the same direction, while adjacent gauges tend to cancel each other for strain in the same direction.

Two Active Gauges Rg with
 R4 Meas Tensile Bending +ε
 R3 Meas Compressive Bending -ε
 R2 Half-Bridge Completion Res
 R1 Half-Bridge Completion Res

Comp for Temperature
 Good Sensitivity to Bending ε
 No Comp for Poisson's (Lower ε)

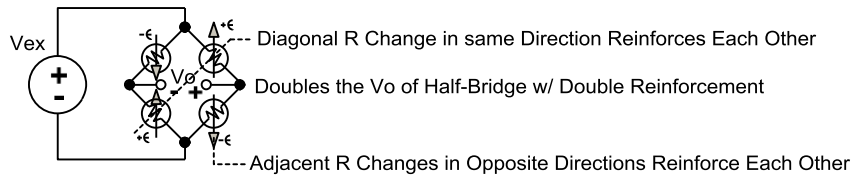
Strain Bridge Equations...

Full-Bridge Type I, N=4 Bending Strain Only (Bending Beams or Shafts Subject to Torsion at Lower Strain Levels)

Four Active Gauges R_g with
 R4 Meas Tensile Bending $+\epsilon$
 R3 Meas Compressive Bending $-\epsilon$
 R2 Meas Tensile Bending $+\epsilon$
 R1 Meas Compressive Bending $-\epsilon$

Comp for Temperature
 Higher Sensitivity to Bending ϵ
 No Comp for Poisson's (Lower ϵ)

Full-Bridge Type I



The Full-Bridge Type I is common to strain measurement of bending beams or shafts subject to torsion at lower levels of stress. This arrangement utilizes four active gauges with one diagonal pair measuring tensile bending strain and the opposite diagonal pair measuring compressive bending strain for the same applied stress (the diagonal gauge pairs in the same direction and adjacent gauge pairs in opposite directions reinforce each other making this bridge the most sensitive). While having greater sensitivity, it is generally used at lower levels of strain (no transverse mounted Poisson's strain gauges). The full-bridge is balanced with all gauges having the same resistance change, maintaining adjacent $R1/R2=R3/R4$ ratios equivalent over temperature.

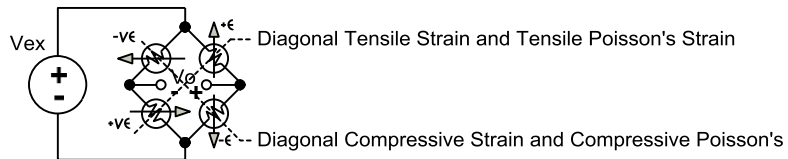
Because the four gauges are arranged to reinforce their effects on V_0 both diagonally and adjacent, the Full-Bridge Type I doubles the V_0 signal of a half-bridge and quadruples that of a quarter bridge. But its greater 2x sensitivity than the half-bridge makes it more expensive because of two additional gauges. Solving for the Full-Bridge Type I strain yields (note the absence of Poisson's strain): $\epsilon = -Vr / GF$.

Full-Bridge Type II, N= 2(1+ γ) Bending Strain Only (Bending Beam or Shaft Subject to Torsion at Higher Strain Levels)

Four Active Gauges R_g with
 R4 Meas Tensile Bending $+\epsilon$
 R3 Meas Compressive Bending $-\epsilon$
 R2 Meas Tensile Poisson's $+\epsilon$
 R1 Meas Compressive Poisson's $-\epsilon$

Comp for Temperature
 Less Sensitive to ϵ than Type I
 Comp for Poisson's (Higher ϵ)

Full-Bridge Type II



Full-Bridge Type II is common to strain measurements for bending beams or shafts subject to torsion at higher stress levels (higher stress drives higher Poisson's strain). This arrangement utilizes four active gauges subject to bending stress, with one diagonal gauge pair aligned to measure tensile bending strain and transverse tensile Poisson's strain (i.e. top of beam), and the other diagonal pair aligned to measure the coincident compressive strain and transverse compressive Poisson's strain (i.e. bottom of beam). Solving for the Full-Bridge Type II strain yields: $\epsilon = -2Vr / [GF*(\gamma + 1)]$.

Strain Bridge Equations...

Full-Bridge Type III, $N = 2(1 + \gamma)$ Axial Strain Only (Single-Axis Column Strain)

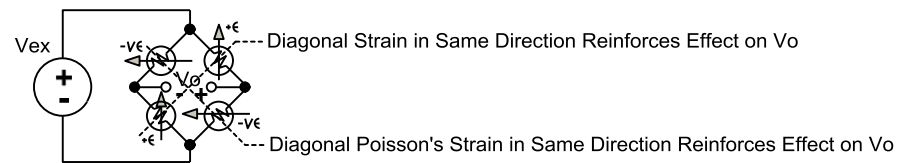
Four Active Gauges R_g with
 R4 Meas Tensile $+\epsilon$
 R3 Meas Compressive Poisson's $-\epsilon$
 R2 Meas Tensile $+\epsilon$
 R1 Meas Compressive Poisson's $-\epsilon$

Comp for Temperature
 Comp for Poisson's (Higher ϵ)

Sensor Gauge Factor and Instrument Gauge Factor

Example: If measured strain
 $\epsilon = 1000$ micro-strain and $GF = 2.00$.
 Then, $2.00 * 1000 * 10^{-6}$ strain
 $= 0.002 = (\Delta R/R)$ and this implies a
 350Ω gauge changes its resistance
 by only 0.2%, equivalent to 0.7Ω .

Full-Bridge Type III



The Full-Bridge Type III is common to column stress measurement applications. This arrangement uses four active gauges subject to a uniaxial stress, with one diagonally opposite gauge pair measuring the principal axial strain in one direction (one mounted on top, one on bottom), and the other diagonal pair measuring the transverse Poisson's strain in the same direction (one mounted transverse on top and other transverse on bottom). Solving for the Full-Bridge Type III strain yields:

$$\epsilon = -2V_r / [GF * (\gamma + 1) - V_r * (\gamma - 1)].$$

Because the Full-Bridge Type III configuration includes measurement of coincident Poisson's strain, it is suitable for measurement at higher stress levels above $5000\mu\epsilon$.

The sensor Gauge Factor GF of a strain gauge is a characteristic transfer coefficient that relates the gauge element sensitivity to strain ϵ relative to its change in resistance ΔR . More specifically, GF is the ratio of the fractional change in resistance to the strain ($GF = (\Delta R / R) / (\Delta L / L) = (\Delta R / R) / \epsilon$). The Gauge Factor for metallic strain gauges is typically around 2.00, but may vary with temperature, strain level, and gauge mounting, and these application effects will contribute to error in making ideal strain measurements. Think of GF as a built-in scaling factor for the computation of ideal strain that is generally fixed to a value by the gauge manufacturer.

You can think of Instrument Gauge Factor IGF similarly, except it is controlled by you and used to rescale the Indicated Strain of an instrument to help overcome less than ideal application sensor irregularities that may skew strain from its ideal. That is, IGF is usually adjusted as required to make the indicated strain of the instrument converge to an ideal or simulated strain during the process of strain gauge bridge shunt calibration. Optionally, a second means of rescaling Indicated Strain is by using Software Gain. The need to rescale the indicated value of an instrument is largely driven by the inherent lack of precision in applying the strain gauge and the wide variation incurred in the multitude of its applications, and sometimes even between sensors of the same type. Consider, the rated output (mV/V) of a strain gauge may vary by as much as $\pm 10\%$ from its manufacturer specification and between sensors. Rescaling the instrument's indicated value for a given sensor by varying its Software Gain and/or Instrument Gauge Factor allows you to account for this tolerance by trimming your response to more accurately reflect ideal strain in your application. Typically, during shunt calibration, the indicated strain measurement is modified by varying Instrument Gauge Factor and/or software gain to make it reading match a calculated ideal or simulated strain. The simulated strain is calculated using the sensor Gauge Factor specification and a fixed gain of 1, while indicated strain uses the Instrument Gauge Factor and/or Software Gain other than 1. The Instrument Gauge Factor is initially set to 2 (roughly equivalent to the sensor Gauge Factor) and this makes indicated strain roughly equivalent to ideal strain, insofar as much as the application induced error is kept to a minimum.

Resolving Strain or Load

How many active load cells?

One=Quarter Bridge QB
Two=Half-Bridge HB
Four=Full-Bridge FB

Is your strain measurement axial, bending, or torsional/shear?

Which Type best fits the application?

1 active/No Additional=**QB Type I**
1 active+1 Dummy=**QB Type II**

The first step to determining which bridge formulation best fits your application is to identify the number of *active* load cells present or required. An “active” cell means the gauge is mounted so that it will measure tensile or compressive strain in the same direction as an applied force (or transverse for bending strain). A dummy gauge refers to an adjacent matching gauge mounted transverse to the applied force or unbonded to the material such that it is subject to the same temperature, but not mechanically stressed (the ratio of adjacent elements will stay the same over temperature and not affect V_o). A bridge may have one, two, or four strain gauges present, but it is how they are positioned relative to one another and the applied force that will determine their application.

Next you may wish to consider the measurement environment and the relative level of stress you intend to measure. If the environment temperature varies, you can dismiss Quarter Bridge Type 1 which is not temperature compensated. If the strain level you intend to measure is high ($> 5000\mu\epsilon$), then you will want to capture the negative effect of Poisson’s strain on your measurement and consider using Half-Bridge Type I, or Full-Bridge Type II or Type III, which take Poisson’s ratio into account. A simple uniaxial force in one direction may only require one active gauge at lower strain levels, unless the ambient varies, then an adjacent active gauge may be added to temperature compensate the bridge output V_o . If you choose to mount the second gauge transverse to axial strain, then it may additionally capture Poisson’s strain, which will be important at high levels of strain $> 5000\mu\epsilon$ where its contribution becomes significant. If your application needs more output signal (and higher signal to noise ratio), note the Half-Bridge Type II has twice the sensitivity of a Quarter-Bridge, and a Full-Bridge has twice the sensitivity as a Half-Bridge. One active gauge will form a Quarter-Bridge, two active gauges may form a Half-Bridge, and four active load cells may form a Full-Bridge—but the more active gauges you require, the higher your cost.

To determine its Type designation, I, II, or III, you must consider how it is mounted.

If your bridge has one active gauge and no additional dummy gauges or resistive elements present, then you select a **Quarter-Bridge Type I** formulation. If your bridge has one active gauge plus a second passive or “dummy” gauge mounted transverse to the applied stress (for temperature compensation), then you select **Quarter Bridge Type II** formulation. Both Quarter-Bridge types use the same formula for calculating strain and their type distinction simply discerns whether the strain gauge is temperature compensated or not. Both quarter-bridge types also require half-bridge completion resistors (either external or internal) but Type I will require an adjacent fixed “dummy” resistor be connected, while Type II will require an adjacent “dummy” gauge be connected to closely match the temperature coefficient of the active gauge over temperature.

Resolving Strain or Load

1 active+1 transverse= HB Type I	If your bridge has <u>two</u> active gauges, with the adjacent gauge mounted perpendicular to the applied force to measure coincident (Poisson's) strain <u>and</u> to temperature compensate the primary active gauge, then you would select a Half-Bridge Type I formulation, common for measuring uniaxial strain at higher stress levels where the Poisson's strain should be accounted for. Note that the Half-Bridge Type I circuit is like the Quarter-Bridge Type II, except that the transverse mounted gauge is mechanically linked to the material to measure Poisson's strain in addition to temperature compensating the primary active gauge.
1 active+1 opposite= HB Type II	If your bridge has <u>two</u> adjacent active gauges mounted such that they are subject to equal and opposite strains for the same applied force, you would select a Half-Bridge Type II formulation. This is common to bending-beam applications with one gauge is mounted to compress while the other undergoes tension for the same applied force. The presence of the second active gauge also temperature compensates V_0 but does not measure Poisson's strain, making it more accurate at lower levels of strain $< 5000\mu\epsilon$ where Poisson's contribution can usually be ignored.
4 active w/opposite pairs= FB Type I	If your bridge has <u>four</u> active gauges with both adjacent gauge pairs subject to equal and opposite strains for the same applied stress, then you would select a Full-Bridge Type I formulation. This arrangement offers the largest output signal, is inherently temperature compensated, and does not require bridge completion.
1 active \pm pair & 1 transverse pair= FB Type II	If your bridge has <u>four</u> active gauges, with one half of the bridge (adjacent gauge pair) mounted to measure the tensile and compressive strain, and the opposite half mounted to measure their coincident transverse Poisson's Strains, then you would select a Full-Bridge Type II formulation. This type is commonly used to measure the uniaxial stress in bending beam applications. This arrangement is inherently temperature compensated and does not require bridge completion.
1 active tensile pair diagonal + 1 active transverse pair diagonal= FB Type III	If your bridge has <u>four</u> active gauges, with one diagonal gauge pair mounted to measure the principal tensile strain and the opposite diagonal pair mounted to measure its transverse (compressive) Poisson's Strain, then you would select a Full-Bridge Type III formulation. This is commonly selected to measure the strain in a column. This arrangement is inherently temperature compensated and does not require bridge completion and better suited for measuring higher levels of strain where Poisson's contribution is greater.

Table 2 summarizes important features of each of the seven strain gauge bridge types, their common application, the number of active gauges, bridge wiring, bridge sensitivity, any built-in compensation, applicable strain level, plus their strain formulation.

Resolving Strain or Load

Table 2: Salient Features of The Seven SG Bridge Types and Their Strain Formulas

SUPPORT	QB Typ I	QB Typ II	HB Typ I	HB Typ II	FB Typ I	FB Typ II	FB Typ III
Axial	Yes	Yes	Yes	No	No	No	Yes
Bending	Yes	Yes	Yes	Yes	Yes	Yes	No
Shear/Torsion	No	No	No	Yes	Yes	Yes	No
Active Gauges	1	1	2	2	4	4	4
Gauge R Positions & Function	R4 (+ε) R3 Fix R=Rg ² R1,2 HB	R4 (+ε) R3=Dumb Rg ¹ (Transverse) R1,2 HB	R4 (+ε) R3 (-γε) R1,2 HB	R4 (+ε) R3 (-ε) R1,2 HB	R1,3 (-ε) R2,4 (+ε)	R1 (-γε) R2 (+γε) R3 (-ε) R4 (+ε)	R1,3 (-γε) R2,4 (+ε)
³Sensitivity (Vr) @1000με	~0.5mV/V	~0.5mV/V	~0.65/V	~1.0mV/V 2x QB	2.0mV/V 2x HB, 4x QB	1.3mV/V	1.3mV/V
Comp Temp?	No	Yes	Yes	Yes	Yes	Yes	Yes
Comp Poisson's γ?	No	No	Yes	No	No	Yes	Yes
Strain High/Low	Low<5000με	Low<5000με	High	Low<5000με	Low<5000με	High	High
TYPE & N	STRAIN FORMULA & PRIMARY APPLICATION						
QB Typ I N=1	$\epsilon = -4Vr * (1 + RI / Rg) / [GF*(1+2Vr)]$, Axial or Bending strain in a constant temperature environment because its output is not temperature compensated.						
QB Typ II N=1	$\epsilon = -4Vr * (1 + RI / Rg) / [GF*(1+2Vr)]$, Axial or Bending strain in a variable temperature environment, common use in weigh-scale load cells and at lower levels of strain where the effect of Poisson's strain is small.						
HB Typ I, N=1+ γ	$\epsilon = -4Vr * (1 + RI / Rg) / [GF*(1+ \gamma) - 2Vr*(\gamma - 1)]$, Uniaxial tensile or compressive strain in a temperature variant environment and good for higher stress levels where Poisson's strain is more significant.						
HB Typ II N=2	$\epsilon = -2Vr *(1 + RI / Rg) / GF = -4Vr*(1 + RI / Rg) / N*GF$, Bending beam strain with two strain gauges subject to equal and opposite strain for the same applied force.						
FB Typ I N=4	$\epsilon = -Vr / GF = -4Vr / (N*GF)$, Bending beam strain or a shaft under torsion with 4 active gauges arranged to measure equal and opposite strains. 2x the sensitivity of a half bridge, 4x the sensitivity of a quarter bridge. Used at lower levels of strain where the Poisson's effect is small.						
FB Typ II N= 2(1+ γ)	$\epsilon = -2Vr / [GF*(\gamma + 1)] = -4Vr / (N*GF)$, Axial column strain with one adjacent gauge pair measuring principal tensile and compressive strain and the opposite adjacent pair measuring the corresponding transverse Poisson's Strains, good for strain measurement at higher stress levels where Poisson's strain is significant.						
FB Typ III N= 2(1+ γ)	$\epsilon = -2Vr / [GF*(\gamma + 1) - Vr*(\gamma - 1)]$, Axial column strain with diagonal gauge pairs measuring tensile strain and the diagonally opposite gauge pair measuring the coincident transverse compressive Poisson's strain.						

Symbols: +ε is positive or tensile strain and -vε is its compressive Poisson's strain, -ε is negative or compressive strain and +vε is its tensile Poisson's strain, HB refers to Half-Bridge completion resistors.

Notes (Table 2): ¹The quarter bridge resistor R3 is an inactive gauge that is mounted transverse or unbonded to the application material (thermally linked but not mechanically linked). ²The quarter bridge resistor R3 matches the nominal active Rg resistance but is neither thermally linked or mechanically linked to the material that Rg attaches to. ³The sensitivity of a bridge network is measured in mV/V and represents the full-scale output Vo with Vex=1V and is equivalent to Vr=Vo/Vex. Given strain, you can solve the strain equation for Vr to determine sensitivity. ⁴Equations apply for output in the polarities shown. If HB completion is included, you can connect the bridge completion resistors to IN+ instead of IN- to flip the polarity of the bridge output Vo and remove the negative sign preceding each equation.

Example Calculation for a Strain Gauge

A 120Ω strain gage is wired in a quarter-bridge circuit to measure the strain imposed on a beam under stress. The bridge excitation voltage is $V_{ex}=10V$. The sensor gauge Factor GF is 2.0. The bridge output is balanced with no load applied ($V_{o_unstrained} = 0$) and the gauge leads are short with negligible lead resistance. When loaded, the bridge output $V_{o_strained}=3.500mV$ and no tare applies. What is the strain imposed on this beam under load?

First, refer to Table 2 on page 15 to determine the Quarter-Bridge Type designation, I or II – A single gauge with no adjacent dummy gauge forms a Quarter-Bridge Type I circuit and strain $\epsilon = -4V_r * (1 + R_l / R_g) / [GF*(1+2V_r)]$.

Note $R_g=120\Omega$, $R_l=0$, and $GF=2.0$. With $V_o=0.0035$ and $V_{ex}=10V$, we can calculate the strain computation term $V_r = V_o/V_{ex} = 0.0035/10 = 0.00035$ which represents the sensitivity of the strain bridge. That is, using V_r , the calculation of requisite strain is straight-forward using $\epsilon = -4V_r * (1 + R_l / R_g) / [GF*(1+2V_r)] = -4*0.00035 / [2*1.0007] = -699.5$ micro-strain (negative strain is compressive).

How would a digital instrument measure this strain? A modern strain instrument would use an Analog-to-Digital Converter (ADC) and measure both the sensor bridge output V_o and the bridge excitation V_{ex} voltages, typically as 16-bit or greater bipolar digital counts. For the [Acromag TT351](#), the V_{ex} voltage is determined by measuring it relative to a fixed voltage reference V_{ref2} at a gain of gain of 1. The ADC returns a digital count ex_count for V_{ex} using 16-bit bipolar math with $ex_count = V_{ex}*32768/V_{ref2} + 32767$, then solves the expression for the corresponding V_{ex} voltage.

The V_o voltage is measured similarly, but relative to a variable ratio-metric ADC reference V_{ref1} directly related to the V_{ex} voltage. The ADC returns a 16-bit bipolar count according to $V_o_count = V_o * GAIN * 32768 / V_{ref1} + 32767$. The module sets GAIN to 1, 2, 4, 8, 16, 32, 64, or 128 ($\pm V_{ref1} / \pm over-range$). One additional piece of information relative to the gauge is used to set over-range—its gauge Rated Output RO. For this example, the gauge RO is 5mV/V. This means that for a full load with $V_{ex}=10V$, the bipolar $\pm 100\%$ input signal is $\pm 10V * 5mV/V = \pm 50mV$. The Acromag module will set its over-range to 150% of this full-scale range, or by user specification up to 150%. It determine its GAIN by setting it $< V_{ref1} / Over-range$. Then the input count equation is solved for the V_o voltage that corresponds to the digital count returned.

With the V_r computation term for strain (bridge sensitivity) computed as $V_r = V_o/V_{ex}$, the module has all the terms it needs to compute the requisite strain for the Quarter-Bridge ($R_g=120\Omega$, $R_l=0$, and $GF=2.0$, V_o , V_{ex}). To resolve Indicated Strain, it will additionally use Instrument Gauge Factor in place of sensor Gauge Factor and apply any additional user-specified software gain instead of 1 to compute the Indicated value.

Example Calculation for a Load Cell

The load cell is a device principally used in weighing systems that utilizes strain gauge technology internally, but whose output is expressed in equivalent units of force or percent, not micro-strain.

Most load cells will have 4 or 6 leads and already have bridge completion and temperature compensation built-in. Internally, a load cell will contain some permutation of quarter, half, or full-bridge circuitry, but this detail is irrelevant to the load computation and is not usually provided by the load cell manufacturer.

The load cell is a simpler form of Wheatstone Bridge based sensor, but one whose output reading is not expressed in micro-strain, but in common units of measure for pressure or weight (typically percent of full rated load). Unlike the SG input type, processing a load cell signal does not require additional detail of its internal bridge type, its gauge factor, or Poisson's ratio. The only important considerations for load cells are its Rated Output (mV/V), its Excitation level, and its rated capacity.

Example: A compression load cell with six connection wires: sense \pm , excitation \pm , and signal \pm , is specified by its manufacturer as follows (bold specs are required):

- **Rated Output: 2.0mV/V**
- **Rated Excitation: 10V DC (15V Maximum)**
- **Rated Capacity: 50,000 lbs/square-inch**
- Safe Overload Level: 150% of Full-Scale
- Operating Temperature Range: -65 °F to 200 °F

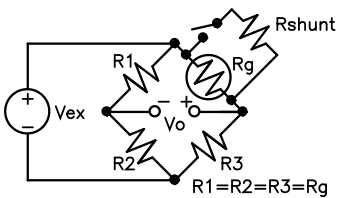
The cell output $V_o = 0.0035V$ and this load contains no offset or tare, what is the indicated load?

Shunt-Calibration of Strain Gauge Bridge

A strain gage instrument that utilizes constant voltage sensor excitation commonly uses Shunt-Calibration to affect its Indicated Strain measurement by adjusting Instrument Gauge Factor and/or Software Gain to make its reading converge with an ideal or simulated strain. This is accomplished by temporarily connecting a precision resistance in parallel with an arm of the Wheatstone Bridge (usually a dummy resistance) to stimulate the instrument’s response to a decrease in resistance corresponding to a known strain (or simulated ideal strain). The use of the term “calibration” is somewhat of a misnomer here because Shunt Calibration does not calibrate the measurement accuracy of the instrument itself to any known standard, but rather the strain bridge sensor it connects to, allowing its Indicated Strain to be scaled to correct engineering units and to overcome excitation and gain error due to tolerance, temperature changes, and other sources of measurement system error (the sensitivity of the sensor-transducer strain measurement system).

Shunt-calibration is the most common approach used to verify the operation of a strain measurement system to detect important changes that may occur over time. Traditionally, some strain gage instrument manufacturers collect and supply shunt calibration data for their instruments to a known shunt-resistor as a feature to facilitate monitoring the integrity of their measurement over time (this data/reference resistor is not a component of the sensor, but the instrument).

A key strain gauge parameter is its sensitivity to strain or Gauge Factor (GF) equivalent to its fractional change in resistance to fractional change in dimension (strain). The GF of common metallic strain gauges is typically ~2.0. Like sensor Gauge Factor represents a gauge’s sensitivity to strain, Instrument Gauge Factor is used to relate the instrument’s sensitivity to the sensor output. Initially, Instrument Gauge Factor is commonly set to 2.0, approximately equivalent to sensor Gauge Factor and its indicated strain will be roughly equal to ideal measured strain. Generally, if the strain sensor Gauge Factor $GF \neq 2$ or its value changes, the Instrument Gauge Factor also changes accordingly. Adjustments are typically made to IGF to get the indicated strain to converge with an ideal or simulated value to help overcome application errors that result from less than ideal conditions in applied strain measurement.



Recall that an unloaded bridge is balanced with $V_o=0$ when $R_1/R_2 = R_g/R_3$. Shunting a bridge element with R_{shunt} reduces its resistance. Likewise, a decrease in R_g or R_2 will drive an increase in V_o (raising V_{o+} and reducing V_{o-}) and simulate negative strain or compression (positive strain is tensile & negative strain compressive). At simulated strains ≤ 2000 micro-strain, the R_{shunt} value and its simulated micro-strain (E_s) are related by the expression: $R_s = [R_g * 10^6 / (GF * N * E_s)] - R_g$.

Shunt-calibration does not have to shunt the active-gauge R_g of the bridge and it is often more convenient to shunt another bridge element, usually a dummy resistor. The magnitude of response is normally the same, but its sign varies according to the element (refer to Figure on page 7). If the indicated measurement differs from the ideal or simulated value for the applied reference-shunt, the instrument’s gain and/or sensitivity (Instrument Gauge Factor) is adjusted until the Indicated Value values converges with an ideal simulated value.

R_g refers to the resistance of the shunted gauge arm. Nominal bridge resistances are typically 120Ω , 350Ω , or 1000Ω and N is a factor used to account for the presence of multiple active gauges in a bridge circuit (see table below). E_s refers to the simulated strain in micro-strain units (its sign is often omitted because it’s always negative). Note that GF refers to the sensor Gauge Factor--not the Instrument Gauge Factor used to calculate indicated strain.

N	Bridge Type
1	Quarter Bridge Type I & II
$1 + \gamma$	Half-Bridge Type I
2	Half-Bridge Type II
$2 * (1 + \gamma)$	Full-Bridge Type II & III
4	Full-Bridge Type I

The factor N can be used to correct the strain simulated via a strain indicator calibrator (you typically divide the calibrator’s “dial” indication by N to get the actual strain seen by the module with its configuration set to the corresponding bridge type). To calculate **simulated strain** (E_s) in micro-strain units, solve the equation for E_s as follows:

$$E_s \text{ (micro-strain)} = - R_g * 10^6 / (GF * N * (R_s + R_g)).$$

Shunt Calibration of Strain Gauge Bridges...

If the lead-wire resistance R_l happens to be sufficiently large compared to shunt resistance R_s such that $100 \cdot R_l / R_s > 0.1 \cdot$ (*required calibration precision in percent*), then the following calculation for R_s is more precise (note the additional term): $R_s = [R_g \cdot 10^6 / (GF \cdot N \cdot Es)] - R_g - 2 \cdot R_l$. For these equations to be used, it is assumed the resistance of each bridge leg is equal and the bridge is *balanced* prior to performing shunt calibration. Because simulated strain results from R_g shunted by R_s to lower its resistance, this simulates negative strain (compressive) and the sign is sometimes omitted.

IMPORTANT: Shunt Calibration should only be performed on unstrained sensors after nulling any unloaded offsets and without including tare. Unloaded bridge offsets should be nulled and the instrument allowed to warm up several minutes prior to performing shunt calibration.

Sensor Load Cell Calibration

Much like Shunt-Calibration of Strain Gauge Bridge inputs, Load Calibration of Load Cells can be done. Load Calibration does not calibrate the instrument itself, but the load cell it connects to, by rescaling the indicated load using only Software Gain (load cells do not usually disclose their internal Gauge Factor).

Through Load Calibration, the ideal Simulated load and Indicated load are driven to converge by making small adjustments to Software Gain to compensate for gain and excitation tolerance and temperature error. It is the indicated value of load that drives the transmitter output current or voltage signal inclusive of any unloaded offset and tare correction.

IMPORTANT-NULL FIRST: Null any unloaded load cell offset to zero and allow the instrument module to warm-up several minutes prior to attempting Load Calibration. Note that load measurement during load calibration should not include any defined tare.

About Acromag

Acromag is a leading manufacturer of [signal transmitters](#) and conditioners for use with many types of process sensors that will generally amplify and isolate the sensor signal and convert it into a proportional current or voltage output, or [Modbus](#), [Profibus](#), [Ethernet](#) message for interface to a PC, PLC, DCS, or other control equipment. Acromag has designed and manufactured measurement and control products for more than 60 years and are an AS9100 and ISO 9001-certified international corporation with their world headquarters near Detroit, Michigan serving a global network of sales representatives and distributors. Acromag offers a complete line of industrial I/O products including a variety of process instruments, signal conditioners, and distributed fieldbus I/O modules that are available with a 2-year warranty. Industries served include chemical processing, manufacturing, defense, energy, and water services.

For more information about Acromag products, call the Inside Sales Department at (248) 295-0880. You may e-mail sales@acromag.com or write Acromag at 30765 South Wixom Road, Wixom, MI 48393 USA. Please visit our web site at www.acromag.com to learn more.

Bruce Cyburt, Senior Design Engineer, Acromag, Inc., July 12, 2002

Revision History

Release Date	Version	EGR/DOC	Description of Revision
12-JUL-2002	A	BC/KK	Whitepaper: Introduction to Strain & Strain Measurement
26-FEB-2019	B	BC/AP	Update content and remove 851T references.